

# NEP and NET

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# Photon Noise

- CMB experiments today are effectively photon noise limited, i.e., limited by the random arrival times of the photons we are measuring

$$n = \frac{\eta}{\exp(h\nu/kT) - 1} = \left[ \frac{\text{photons}}{\text{s Hz}} \right]$$

- At 150 GHz for a 20 K RJ source, with 0.30 efficiency:

$$\frac{h\nu}{k_B T} = \frac{6.626 \cdot 10^{-34} (150 \cdot 10^9 \text{ Hz})}{1.38 \cdot 10^{-23} (20 \text{ K})} \sim 0.3$$

$$n \approx \frac{0.3}{1 + 0.3 - 1} \sim 1 \frac{\text{photons}}{\text{s Hz}} \text{ per mode}$$

- So for 30 GHz bandwidth  $\rightarrow 3 \times 10^{10}$  photons / sec, i.e., we are measuring lots of photons per sec.

# Noise Equivalent Power (NEP)

- Variance in photons will be:

$$\langle \Delta n^2 \rangle = n + n^2$$

- Variance in the photon power will be:  $(h\nu)^2 \langle \Delta n^2 \rangle$

- The noise equivalent power will be the variance in the photon power, for two polarization modes, integrated over frequency, per 1 sec of integration:

$$NEP_{\gamma}^2 = \int 4(h\nu)^2 n d\nu + \int 4(h\nu)^2 n^2 d\nu = [W^2 / Hz]$$

- Power is  $P_{\nu} = 2nh\nu$ , so can re-write above as:

$$NEP_{\gamma}^2 = \int 2h\nu P_{\nu} d\nu + \int P_{\nu}^2 d\nu$$

- First term is “Poisson” term, and the second term is the “Bunching” term, due to correlated nature of photons emission

# Photon Noise (NEP)

- Assuming spectrum does not vary significantly over band, NEP can be approximated as:

$$NEP_{\gamma}^2 \approx 2P_{opt}h\nu_0 + P_{opt}^2/\Delta\nu$$

- For our 150 GHz detector with 40 GHz bandwidth and 6.5 pW of loading, this gives:

$$NEP_{\gamma}^2 \approx 1.26 \times 10^{-33} + 1.06 \times 10^{-33} [W^2/Hz]$$

- Poisson and bunching terms are approximately equal, which is not that surprising consider that is  $n \sim 1$  (i.e.,  $n \ll 1$  infers Poisson term dominates,  $n \gg 1$  infers bunching term dominates)

$$NEP_{\gamma} \approx 4.8 \times 10^{-17} [W/\sqrt{Hz}] = 48 [aW/\sqrt{Hz}]$$

# ***Thermal Carrier (“G”) Noise***

- The detector has an intrinsic noise from thermal fluctuations across the thermal link, often called “G” or “Phonon” noise:

$$NEP_G^2 = 4k_B T_b^2 G$$

- To design a bolometer want the following properties:
  - 1) Design “G” to match expecting loading (Popt)
  - 2) Make band-width x efficiency product as large as possible
  - 3) Keep G-noise < Photon-noise
- Yesterday, said that typical parameters are  $G \sim 100 \text{ pW/K}$  and  $T_b \sim 0.5 \text{ K}$ , which implies:

$$NEP_G \approx \sqrt{4k_B (0.5K)^2 (100pW/K)} \sim 37 [aW/\sqrt{Hz}]$$

- On order of photon noise. In practice, try to tune  $G/P_{\text{sat}}$  or  $T_c$  as low as possible, to minimize G-noise.

# *Readout Noise*

- Readout noise also can contribute to system noise.
- For example, SQUID noise is usually quoted in Noise Equivalent Current (NEI) as  $\sim 4$  pA/sqrt(Hz).
- To convert to NEP need to multiply by voltage bias of detector, typically  $\sim 4$  uV for a 1 Ohm detector (Pelec  $\sim 15$  pW), i.e., the SQUID will provide NEP  $\sim 16$  aW/sqrt(Hz)
- Rule of thumb: smaller voltage bias will typically reduce size of readout noise when referenced to bolometer:
  - e.g., main reason why many groups design TES with smaller resistances  $\sim 30$  mOhm, to keep voltage bias as small as possible.

# ***NEP to NET (Noise-Equivalent Temperature)***

- Need to convert NEP to noise-equivalent temperature, i.e., how big a power fluctuation on the bolometer we would expect for given temperature fluctuation:

$$NET = NEP \frac{dT}{dP}$$

- Easy to do in RJ limit:

$$P_{RJ} = 2k_B T_{RJ} (\eta \Delta \nu)$$

$$\frac{dP_{RJ}}{dT_{RJ}} = 2k_B (\eta \Delta \nu) \sim 2k_B (0.3 \times 40e9)$$

- Implies that:

$$NEP \approx 50 \text{ aW} / \sqrt{\text{Hz}} \longrightarrow NET_{RJ} \approx 150 \text{ } \mu\text{K} / \sqrt{\text{Hz}}$$

# ***NEP to NET (Noise-Equivalent Temperature)***

- More helpful to work in CMB units, using blackbody equation:

$$B(\nu, T) = \frac{2h\nu^3}{c^2} \frac{1}{\exp(h\nu/kT) - 1} \quad x = \frac{h\nu}{k_B T_{CMB}}$$

$$\frac{dP}{dT_{CMB}} = 2k_B(\eta\Delta\nu) \frac{x^2 e^x}{(e^x - 1)^2}$$

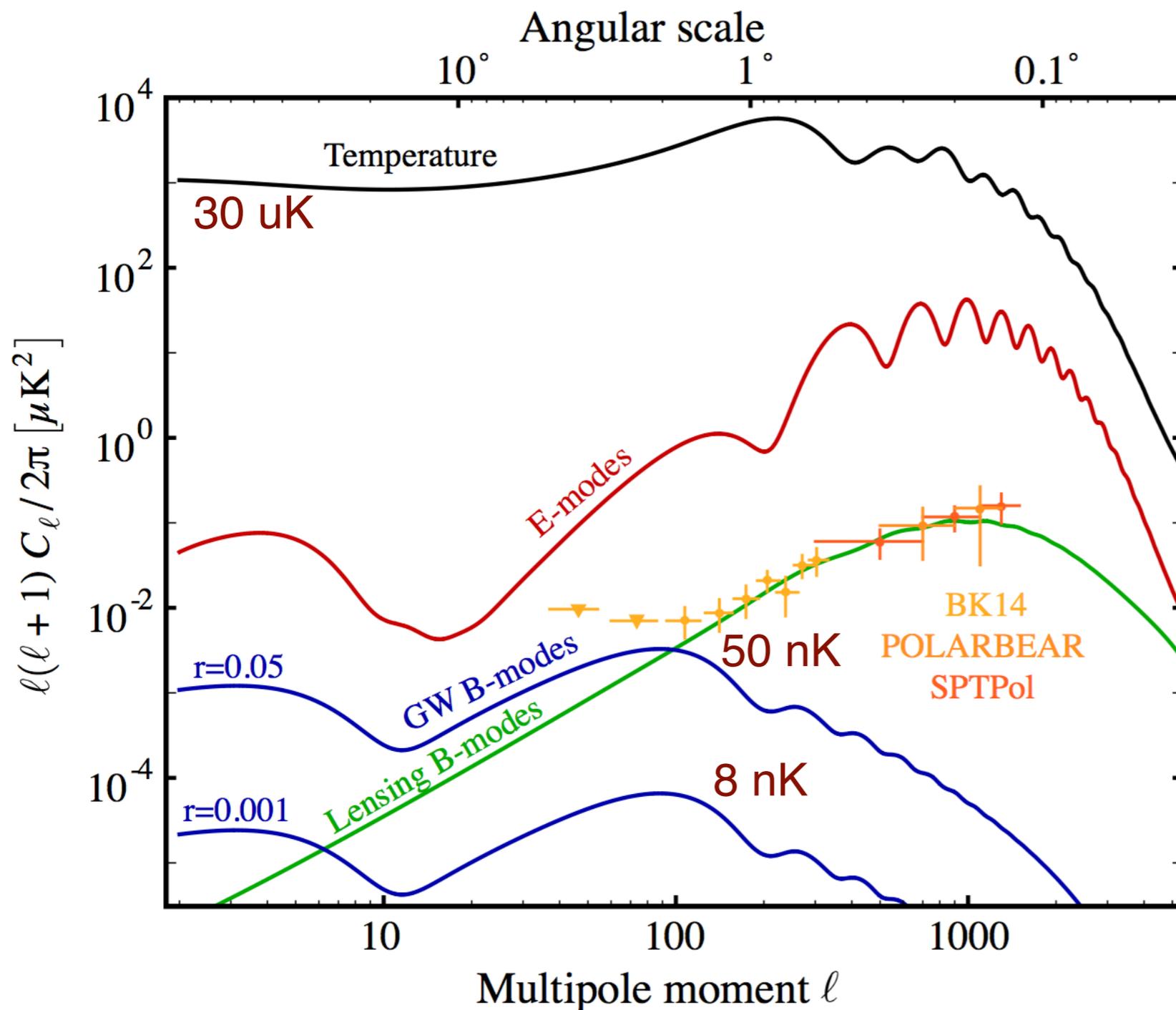
- At 150 GHz with  $T_{cmb}=2.725$ , implies  $x = 2.64$ , and:

$$NEP \approx 50 \text{ aW}/\sqrt{\text{Hz}} \longrightarrow NET_{CMB} = 262 \text{ } \mu\text{K}/\sqrt{\text{Hz}}$$

- Conversion between RJ and CMB temp at 90, 150, 220 GHz are factors of  $\sim 1.23$ ,  $1.74$ , and  $3.08$ , respectively, i.e., correction gets larger the further away from RJ part of spectrum.

# Designing CMB-S4

- One of primary goals of CMB-S4 is to detect inflationary gravity waves through B-mode spectrum.



- Power spectrum gives you sense of how big the signals you are looking for.
- In temperature, large-scale anisotropies correspond to 30 uK RMS (i.e., 1/100,000 of  $T_{\text{cmb}}$ )
- Peak in B-mode spectrum at  $\ell \sim 80$  corresponds to 50 and 8 nK signal for  $r = 0.05$  and  $r=0.001$ , respectively.

# *How many detectors do we need?*

- NET per detector tells us size of fluctuation we can see in a unit observing time. Assume polarization sensitive detectors (i.e., NET increases by  $\sim\sqrt{2}$ , and convert  $1/\sqrt{\text{Hz}}$  to  $\sqrt{\text{sec}}$  by dividing NET by  $\sqrt{2}$ )

$$NET_{\text{bolo}} \approx 260 \mu\text{K} \sqrt{s}$$

- Useful measure of sensitivity of the map for B-modes is nK-deg, i.e., what is the RMS of the map on 1-deg scales

$$\text{Noise}_{\text{map}} [n\text{K deg}] \approx \frac{NET_{\text{bolo}} \sqrt{\text{SkyArea}(\text{deg}^2)}}{\sqrt{N_{\text{bolo}} t}}$$

- Inflationary B-mode signal peaks at  $\sim 1$ -deg, so we want to get down to at a level such that image fluctuations with  $S/N \sim \text{few}$ , i.e., to get  $\sigma(r) \sim 0.001$  need noise  $\sim 8$  nK-deg / 3  $\sim 3$  nK-deg

# How many detectors do we need?

$$Noise_{map} [nK deg] \approx \frac{NET_{bolo} \sqrt{SkyArea(deg^2)}}{\sqrt{N_{bolo} t}}$$

- Sky Area: All-sky is  $\sim 40,000 \text{ deg}^2$ , typically thought we should focus on smaller patch with clean foregrounds  $\sim 2000 \text{ deg}^2$
- Observing time: 1 year =  $3 \times 10^7 \text{ sec}$ , lets just assume a 4-yr survey with 25% obs. efficiency (close to typical)

$$N_{bolo} = \left( \frac{300 \mu K \sqrt{s}}{0.003 \mu K deg} \right)^2 \frac{2000 deg^2}{3 \times 10^7 s} \approx 600,000$$

- So we expect CMB-S4 to require an instrument with  $\sim$ order half million bolometers